



Ashenhurst's

Cloth Structure Tables

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Compiled on Strictly Scientific Principles by

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PREFACE.

In compiling and publishing these Tables I am fully conscious that I am subjecting myself to the probability of severe criticism. I have done so before. When I published my Tables of Diameters of Threads, as far back as 1884, I incurred the same risk, but every subsequent writer, some with, others without acknowledgment, have adopted them or deductions made from them, and no one has yet to my knowledge, challenged their accuracy.

In working out these Tables I have endeavored to give the number of threads per inch which will produce the most perfect cloth under average conditions, and I have based my calculations upon observations of the best fabrics, covering a period of over twenty years.

Of course the conditions which apply to one pattern will not necessarily apply to all patterns. The process of finishing and other conditions come in as factors, and it would be impossible to frame either rules or tables which would apply equally to all cases, but I have endeavored to meet this by giving in each combination of counts the number of threads which will give the best cloth under the conditions for which they are calculated, that is permitting the greatest amount of curvature in the weft and the least in the warp, and varying them as the ratio of the counts used vary, but I have also worked out the lowest and the highest possible number of threads which may be used in such combinaion, so that the manufacturer may know how far we may go in either direction without destroying the stability of structure or making his cloth too stiff or rigid to use for the purpose for which it is intended.

The accompanying rules as to the number of picks per inch of weft, twist of yarn, alteration of weights, etc., are intended to assist in the production of perfect cloths, or as near perfect as the conditions under which they may be produced, such as price, weight, etc., will permit; and at the same time to save intricate calculations and the experiments which enevitably accompany the making of samples when the true laws are not clearly understood.

Years of experiment with known cloths have proved that the basis upon which they are compiled is the truest and that they may prove useful and reliable is the only wish of the author.

THOS. R. ASHENHURST.



Ashenhurst's Cloth Structure Tables.

THE USE OF THE TABLES.

The primary object of these Tables is to enable a manufacturer, superintendent of a mill, designer or any one to whose care the production of fabrics is entrusted to produce a fabric perfect, or as near perfect as possible, and both the Tables and Rules are framed with a view to meeting that object.

The general instructions on the sheets themselves will show their uses. For instance: take any one of the tables and find the counts of warp at the head of the column, and the counts of west at the side. both of which are proposed to be used, and running along both the horizontal lines and vertical columns the square corresponding with the two will give the minimum number of threads which may be used in a plain cloth of those two counts in the left hand top corner; the maximum which may be used in the right bottom corner, and that which will give the most perfect structure in the center, and in .heavier type; so that an increase or decrease in weight may be made without risk of destroying the qualities of stability on the one hand or making the cloth too stiff or rigid on the other. The Tables apply to the warp threads only, as considerably more latitude may be, and is, given in the weft threads for many reasons, but the accompanying rules will explain more than a general description:

Table A is for Worsted Warp and Worsted Weft.

Table B.—Cotton or Spun Silk Warp and Weft.

Table C.—Cotton or Spun Silk Warp and Worsted Weft.

Table D.-Woolen Warp and Woolen Weft.

Table E.—Cotton or Spun Silk Warp and Woolen Weft.

Then, as already explained, find the square corresponding to the counts of the two yarns to be used, on the tables referring to the two materials and the numbers of ends per inch for minimum, maximum and perfect structure will be found for a plain cloth.

TO CHANGE PATTERN.

When any other than a plain cloth is to be made there must be a change in the number of threads. There are two rules: one a rough and ready method which gives some approximation to truth and the other a strictly true and scientific method. Suppose a four thread twill cloth is to be made, weft passing over two and under two warp threads alternately, as sometimes expressed thus, 25. The pattern will consist of four threads and there will be two points of intersection of weft with the warp. Then if both materials are of the same counts the general rule would be to take a common proportion. Suppose that 52 ends would give perfect structure for plain cloth. Thus 4 threads +2 intersections =6, as against 4 threads + 4 intersections in plain cloth. Therefore as 6:8::52:69.3. This is not strictly true as in working out the tables a suitable allowance has been made for the bending of the threads in the cloth, consequently the number of threads per inch given in the table represents so many triangles, including both the diameter of the warp thread and the weft thread, as well as the space required for the proper degree of beiding; hence the correct method in changing the pattern is to take each intersection in the pattern as a triangle whose base is represented as a fraction of an inch and each thread where no intersection occurs at its own diameter only, and add them together to find the space occupied by one pattern, and that multiplied by the number of threads in the pattern will give the number per inch. In the present case there are 52 ends of 30s worst d per inch in a plain cloth to change to a four end twill, so that each angle or intersection is $\frac{1}{32}$ of an inch. The diameter of this thread is $\frac{1}{130}$ of an inch, thus two threads and the bases of the two triangles will be $(\frac{1}{130} + \frac{1}{130}) + (\frac{1}{52} + \frac{1}{52}) = \frac{1}{63} + \frac{1}{63}$ $\frac{1}{26} = \frac{65 \times 26}{65 \times 26} = \frac{1}{18.57}$ of an inch, the space occupied by one pattern, and as there are four ends in the pattern $18.57 \times 4 = 74.28$ ends per inch for the twill cloth as against 52 in the plain one. This rule will work out correctly for every pattern, whatever the counts or combination of counts may be, when the pattern is an ordinary twill ruuning at an angle of 45 degrees, not necessarily in the cloth but on

paper, or in other words where the pattern moves one end at each succeeding pick. Where such is not the case the conditions will be altered as will be shown.

WHEN WARP OR WEFT PREDOMINATES ON THE SURFACE.

Whenever the warp or weft predominates largely on the surface in the order of interweaving, as in satins, or when the twill runs at an angle of 60 degrees or more with the warp or weft, then there must be more warp if the twill is in the direction of the warp, either thicker threads or more of them, than would be used for an even twill at an angle of 45 degrees. If the twill runs across the piece at an angle of 30 degrees or less then the weft must predominate, just as with a warp face satin there must be more warp than weft, and a weft-face satin the reverse, and it is better to have that material which predominates on the face fine and a proportionately large number of threads. It is impossible to lay down a rule to apply to every pattern but it may serve in a general way that for a five thread satin or twill ± that the maximum number to make a good cloth would be 75 per cent of the number of threads which would lie side by side in one inch as given in the accompanying Table of Diameters: Following the strict rule as laid down for, say a cotton warp and weft satin, warp on the surface, counts of warp $\frac{1}{30}$ s and weft 36s then there would be two intersections in the five threads composing the pattern, and as for a plain cloth 33 ends per inch gives the best structure there would be $(\frac{1}{36} \times 2)$ $+ (\frac{1}{204} \times 3)$ to find the number of patterns per inch, $(\frac{1}{204})$ in the diameter of 50s cotton) hence there would be 21.52 pattern per inch, and 21.52 \times 5 = 107.6 ends per inch; or to take the maximum given in the tables $(\frac{1}{84} \times 2) + (\frac{1}{204} \times 3) = 25$ patterns per inch and $25 \times 5 = 125$ ends per inch. It is better to work by mean in the tables than go to the extremes for the purpose of retaining flexibility. A satin may be made with as many ends per inch as would lie side by side, but it is generally undesirable.

TO FIND PICKS PER INCH.

In a plain cloth, or twill cloth, where warp and weft are equal in counts and material, there should be approximately the same number of picks as ends per inch. In practice it is often better to have the weft a little thicker than the warp. In other cases where the two materials are not the same, or where pattern becomes an element in the case, make the basis one half the number of threads which would lie on one inch as given in the tables of diameters, and add or deduct 10 per cent for the maximum or minimum, except in cases such as already referred to of satins or patterns with a weft surface, and low angled twills, where the threads must lie as closely together as possible.

FANCY CLOTHS WITH YARNS OF DIFFERENT COUNTS.

In many cases cloths are made with yarns of different counts or different materials; in such cases the best method is to find the average count of the combination and then refer to the tables. If the two materials are different they must be reduced to the same denomination. Thus suppose 2-40s cotton and 2-36s worsted are being used in combination with equal number of threads in the pattern, thus: 2-40s cotton is $\frac{2.0 \times 8.40}{3.0.0} = 30$ s worsted (single), and 2-40s worsted combined with 30s would give an average count of 24 s. (See rule for finding average count, page 14.)

This rule may be applied in almost all cases of fancy goods.

TO CHANGE THE WEIGHT OF A CLOTH.

A cloth may be altered in weight, made heavier or lighter, and the same character of structure retained. In doing this the fact must be borne in mind that the diameter of threads vary in the ratio of the square root of the counts; hence the rule will be:

Rule:—As the weight of the required cloth is to the weight of the given cloth, so is the square root of the counts in the given cloth to the square root of counts in the required cloth.

This is the true rule, but it may be simplified in

working by squaring the weights, so as to raise them to the same power as the counts and avoid extracting roots. Thus the rule will be: as the weight squared of the required cloth is to the weight squared of the given cloth, so is the counts of the given cloth to the counts of the required cloth.

Example: A cloth is made with 24s warp, in any material and it is desired to increase the weight by one eighth. Then the heavier cloth will bear to the lighter one the ratio of 9 to 8; hence as $9^2:8^2::24:X$, or $\frac{8\times 8\times 2}{9\times 9} = 19$, nearly; or that would be the counts required. The number of ends per inch must now be found, for a heavier count must have fewer threads. Then suppose the original cloth had 56 ends per inch it would be as 9:8::56:X or $\frac{8\times \frac{5}{9}6}{9} = 49\frac{7}{9}$ for the heavier cloth.

It must always be borne in mind that light cloths are fine, and heavy cloths are coarse; that is, thicker threads and fewer of them for the same structure.

TO CHANGE FROM ONE COUNT TO ANOTHER AND FIND ENDS OR PICKS PER INCH.

This is simply a part of the last rule or a reversal of the last portion and will read: "As the given count is to the required count, so are the ends of the given cloth squared to the ends of the required cloth squared."

Example: If there are 56 ends per inch of 24s and it is desired to change to 19s how many ends per inch should there be? Then as $24:19:56^2:x^2$, or $\sqrt{1925}6856=50$. or there would be 50 ends per inch. There is a slight error between 50 and 49 $\frac{\pi}{3}$ given in the previous example due to the fact that the first part of the previous illustration gave a little less than 19, but the full number was adopted.

If it is required to change from one number of threads per inch to another, the above rule would simply be reversed, that is: As the ends of the given cloth squared is to the ends of the required cloth squared, so is the given counts to the required counts, thus reversing the above example as $56^2:50^2:24:19$, or $\frac{5.08503824}{5.083824}=19$.

TO CHANGE FROM ONE PATTERN TO ANOTHER AND FIND ENDS TO PRODUCE CLOTH OF THE SAME CHARACTER.

In the alteration of pattern the simple general rule turns upon the relative number of intersections in proportion to the number of threads in each pattern respectively. Thus a four end twill $\frac{2}{2}$ has four threads and two intersections, and a six end twill $\frac{3}{3}$ has six threads and two intersections, and a plain cloth has six threads and six intersections; hence, a four end twill cloth must contain more threads of the same counts than a plain, and a six end twill must contain more than a four.

If the cloth in the first instance has been made on the basis of these tables the second may be also with the same result; but if not, and the same character of cloth is required a general rule must be laid down.

Then taking the four and six end twills for the purpose of illustration, and supposing the four end twill had 80 ends per inch, to find the number required for the six end twill. In the first cloth as mentioned there are four threads and two intersections, or six units; in the second, six threads and two intersections, or eight units; therefore if the first cloth had 80 threads per inch the second would have $\frac{8.0 \times 4 \times 8}{4 \times 8} = 90$ threads per inch.

To make the matter more clear it may be given in the general rule, viz: As ends in the pattern of the cloth given multiplied by ends, plus intersection, in the pattern of the required cloth, is to the ends in the pattern of the required cloth, multiplied by ends, plus intersection in the pattern of the given cloth, so is the ends per inch of the given cloth to ends per inch of the required cloth.

Then to change from the four end twill with 80 ends per inch it would be:

As $4 \times (6+2) : 6 \times (4+2) : 80 : 90$, or simplified $\frac{6 \times (4+2) \times 80}{4 \times (6+2)} = \frac{6 \times 6 \times 80}{4 \times 8} = 90$ The latter method is the simplest form of working, but the first rule explains the reason for it.

COUNTS OF FOLDED YARN.

To find the counts of a yarn composed of two threads twisted together the doctrine of combinations is employed. Let two threads A, B be twisted together then $\frac{A \times B}{A+B} = X$ the resulting count. Thus if the threads are 20s and 40s respectively in any material it would be $\frac{20 \times 40}{20+40} = \frac{800}{60} = 13\frac{1}{3}$, the counts.

To find one count to twist with a known count and produce a given count in the combination, the rule will be reversed. Thus let C be the resulting counts, then $\frac{A \times C}{A - C} = B$, the single count sought, as $\frac{20 \times 13\frac{1}{3}}{20 - 13\frac{1}{3}} = 40$.

When three or more threads are twisted together the combination is extended. Let the threads A, B, C be twisted together and D the resulting counts, then $(A \times B) + (A \times C) + (B \times C) = D$. Suppose A, B, C to be 40s, 30s and 20s respectively then $(40 \times 30) \times (40 \times 20) + (30 \times 20) = 9\frac{3}{13}$.

The rule may be reversed in the same manner as the others. Thus let A, B, D be given to find C. Then $\frac{A \times B \times D}{(A \times B) - (A \times D) - (B \times D)} = C, \text{ or } \\ \frac{40 \times 30 \times 9_{13}^3}{(40 \times 30) - (40 \times 9_{13}^3) - (30 \times 9_{13}^3)} = 20s.$

When there are more than 3 threads the same rule will follow, the combinations on the under side of the line being always one less than the total number of threads. Thus if there are four threads A, B, C, D it will be

$$\frac{A \times B \times C \times D}{(A \times B \times C) + (A \times B \times D) + (A \times C \times D) + B \times (C \times D)}$$
and so on.

AVERAGE COUNTS.

The object of this rule is when fancy goods are being made to find the number of threads to make a perfect cloth. Suppose a cloth is made of one thread of 40s and one of 20s alternately. The cloth could not be built on either of them separately. Then the rule given above will find the resulting counts of the combination as $13\frac{1}{3}$ s, but that implies that the two threads have been twisted and made into one, but being put into the cloth separately there are still two threads then $13\frac{1}{3}$ X $2=26\frac{2}{3}$, the average counts, and upon this the cloth may be built.

The same rule will apply when there are three or more threads; find the resulting counts of the combination and multiply by the number of threads; the product will be the average counts.

TWIST OF YARNS.

In the cotton trade there is a general rule for finding the twist in a given count, viz: Multiply the square root of the count by 3½ for weft and by 3½ for warp. This is considered as standard yarn, and may be increased or decreased in yarns for specific purposes.

To make a similar standard for other materials as the relative counts are to each other, so is the relative twist. For instance cotton and worsted have 840 and 560 yards per hank respectively. Thus $3.25 \times 560 = 3.25 \times 2 = 2.166$ for weft and

, 3. 75×560 = 2.5 for warp, and the same with any other material.

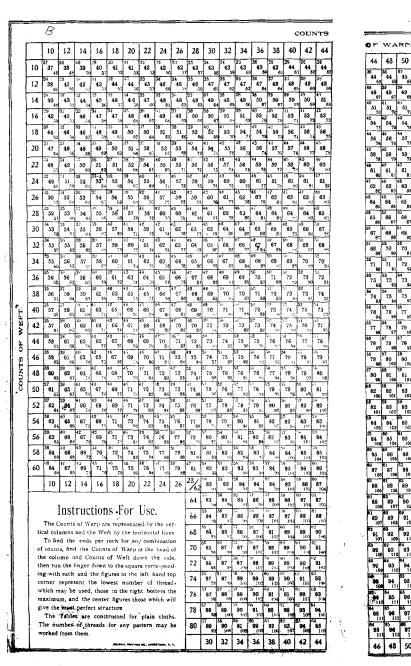
Suppose a yarn is made with either more or less twist than this rule will give and it is desired to make another yarn of exactly the same character, then the general rule will apply. As the square root of one count is to the square root of another count so is the twist in one yarn to the twist in another. Or, as one count is to another count so is the twist of one squared to the twist of the other squared.

Example: Let a 20s yarn have 12 turns per inch how many should a 30s have? As $\sqrt{20}$: $\sqrt{30}$: :12: X or as $20:30::12^2:X^2$, or $\sqrt{\frac{30 \times 12 \times 12}{20}}$ 15, nearly. or the number of turns required for 30s.

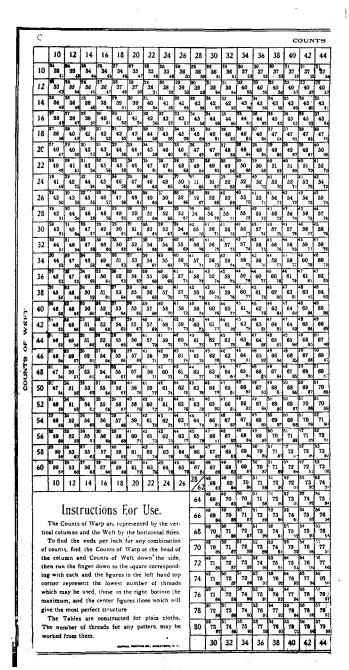
as' they are ns for cloth d not given s number of **DIAMETERS** DIAMETERS DIAMETERS 0F 0F 0F COTTON WORSTED WOOLEN THREADS. but given as' tall calculations for any thread no: will be the nu THREADS. THREADS. American Run System. DIAMETERS DIAMETERS COUNTS DIAMETERS o or the thought of an inch, but in all co find the diameter of an et h, and the answer wi $\overline{49}$ $1\frac{1}{2}$ $2\frac{1}{2}$ $\frac{3}{2}$ 80 The diameters should be written as fractions thus it indicates the numbers which would lie side by side is structure they must be treated strictly as fractions. T in the tables extract the square root of the yards threads which will be side by side. $\frac{32}{34}$ $6\frac{1}{2}$ 109.5 116.5 196.5 120-56 70 72 74 76 78

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| | tic | al colu | amns | and th | ie We | ft by | the ho | rizont | al lin | 26 | 68 | 45 69 78 | 69 89 | 70 | 48 71 81 | 72 85 | 72 66 | 73 ₈₆ | 73 85 | | 74 86 | 75 89 | 75 90 | 76 | 76 | 77 | ľ |
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| | th th | e colu en run | nan a the f | nd Co inger | ounts down | of W to the | eit de squai | own ti | he sio respon | de, id- | 72 | 46 70 | 48 71 80 | 72 82 | 48 73 | 73 83 | 74 86 | 74 | 75 | , | 76 | 70 | 76 : 91 | 77 92 | 78 99 | 78 94 | 64 |
| | sn; | then run the linger down to the square correspond- ing with each and the liqures in the left hand top corner represent the lowest number of threads | | | | | | | | οp | 74 | 46 70 | 71 91 | 72 82 | 48 73 84 | 74 74 | 74 94 | 75 | 76 × | | 76 89 | 377 90 | 77 | 78 92 | 78 _{9:} | 55 79 94 | 55 |
| | w | which may be used, those in the right bott-in the | | | | | | | | he | 76 | 71 | 72 | 73 83 | 48 74 84 | 74 | 75 | 76 | 77 | | 77 90 | 77 91 | 53 78 92 | ⁵³ 78 93 | 54 79 | 56 79 95 | 56 |
| | gi | maximum, and the center figures those which will give the most perfect structure | | | | | | | | į | 78 | 46 71 | 47 72 | 73 | 74 | 75 | 76 | 51 76 | 51 77 | | 77 91 | 58 78 92 | 33 79 93 | 79 84 | 56 80 95 | 55 81 95 | 55 |
| | | The Tables are constructed for plain cloths. The number of threads for any pattern may be | | | | | | | | | 80 | 77 72 81 | 47 73 | 48 74 | 75 | 75 | 76 | 31 77 | 12 77 | | 52 78 91 | ⁶³ 79 92 | 54 80 98 | 35 80 94 | 55 81 96 | 56 81 96 | 36 |
| | we | rked | from | them | | g | 41 40 | 10 CO. JAN | | ., | - | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | | 46 | 48 | 50 | 52 | 54 | 56 | : |
| <u></u> | <u> </u> | | | = | | ANUEN | | , co. A4 | | _ | | | | 1 | 1 | <u> </u> | <u> </u> | <u> </u> | 1 | | أحسط | | | | | _ | ۲ |

| · - | |
|---|--|
| OF WARP | |
| 46 48 50 52 54 56 58 60 | ASHENHURST'S |
| 30 30 80 491 31 32 33 34 37 37 38 38 38 39 39 39 10 51 52 52 53 54 56 57 48 | Cloth Structure Tables. |
| 31 32 32 33 34 34 84 35 12 35 55 55 56 56 57 58 59 60 | ciota Structure Tables. |
| 38 94 34 34 35 36 86 86 14 45 45 14 87 58 58 59 60 61 60 62 | For unding the number of threads per inch in a Cloth in any combination of counts or materials, |
| 35 35 36 35 36 36 36 36 38 44 44 45 45 48 46 46 47 48 16 | |
| 38 36 36 36 36 37 37 37 47 47 47 47 48 49 49 18 62 62 63 63 64 64 64 64 65 | |
| 18 48 48 49 49 50 50 50 50 20 | TABLE A. |
| 188 38 38 39 39 80 10 10 10 10 10 10 10 10 10 10 10 10 10 | For Worsted Warp and |
| 38 29 39 39 40 40 40 40 40 50 50 50 50 50 50 50 50 50 50 50 50 50 | Worsted Weft. |
| 39 | |
| 50 51 61 41 42 42 42 42 43 45 55 55 55 56 56 56 56 56 56 56 | 64 66 68 70 72 74 76 78 80 |
| 55 12 12 42 43 43 43 44 44 55 55 56 56 56 57 57 57 58 58 58 58 70 70 70 70 70 70 70 70 70 70 70 70 70 | 58 58 59 59 59 59 59 60 60 60 81 81 81 81 81 81 81 81 81 81 81 81 81 |
| 12 43 43 44 44 45 45 46 58 58 59 73 74 75 75 75 76 77 77 78 | 15 46 46 46 47 47 47 47 48 48 48 59 59 59 60 60 60 60 61 61 61 61 832 |
| 18 13 18 14 14 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16 | 60 60 60 61 61 62 62 62 62 83 33 |
| 48 43 44 44 45 45 45 45 45 45 45 45 45 45 45 | 47 47 48 48 48 49 49 49 49 49 83 83 84 84 88 83 85 85 |
| 46 60 61 62 62 62 63 63 64 81 67 78 79 79 80 80 81 81 | 48 48 48 49 49 49 49 65 50 50 65 88 88 88 88 88 88 88 85 86 86 8 |
| 44 45 45 45 46 47 47 47 65 65 77 80 80 81 81 82 82 | 48 49 49 49 49 30 50 50 50 51 66 65 66 66 67 67 67 88 |
| 15 16 16 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18 | 49 49 50 50 50 50 50 51 51 51 68 42 85 86 86 86 86 87 87 88 89 42 |
| 46 48 46 47 47 48 48 48 49 19 66 79 80 81 81 82 83 84 86 85 | 49 50 50 50 50 50 51 51 51 51 67 67 67 67 68 68 69 44 86 66 66 67 87 87 88 88 89 99 |
| 64 65 65 65 66 66 66 66 67 67 67 80 83 83 84 85 85 85 86 | 50 50 50 51 51 51 52 52 52 67 68 68 68 69 69 69 70 70 70 46 |
| 65 66 66 66 67 67 67 67 68 68 68 87 84 85 86 86 87 | 51 51 51 52 52 52 53 53 53 69 69 69 70 70 70 71 71 71 71 48 88 88 88 89 90 90 91 91 92 |
| 86 67 67 67 68 68 68 69 69 69 80 88 69 87 89 | 69 70 70 70 70 71 71 71 71 72 72 50 |
| 88 68 68 68 68 68 69 69 70 70 83 84 84 85 86 68 69 69 70 70 | 70 71 71 71 72 72 72 72 73 73 73 52 52 |
| 68 69 69 69 70 70 71 71 71 71 | 71 72 72 72 72 73 73 74 74 54 |
| 19 10 10 10 10 10 10 10 10 10 10 10 10 10 | 72 73 73 73 73 74 74 74 75 75 75 75 56 75 96 96 96 |
| 70 70 71 71 72 72 73 73 74 91 95 96 91 91 | 74 74 74 74 74 75 75 76 76 76 76 58 |
| 72 72 72 72 72 73 73 74 74 75 | 75 76 76 76 76 76 76 76 76 77 77 77 77 60 |
| 72 73 73 73 74 74 75 75 75 | 76 94 95 96 96 96 96 96 57 77 78 78 62 |
| 73 73 74 74 75 75 76 78 76 | 54 55 55 56 56 66 57 57 58 78 78 78 78 78 78 79 64 95 94 95 97 97 98 98 99 100 |
| 73 73 74 74 75 75 76 77 77 88 88 89 90 91 92 93 94 94 | 55 55 56 66 57 57 58 58 56 78 78 79 79 98 98 66 66 96 98 97 97 98 98 98 98 98 |
| 74 75 75 76 76 77 77 77 78 78 | 55 56 56 57 57 57 58 58 58 58 68 68 68 68 68 68 68 68 68 68 68 68 68 |
| 61 52 52 53 53 54 54 56 65 79 88 88 90 91 92 93 94 96 96 | 55 56 57 80 80 80 81 81 81 82 70 80 99 100 10 102 102 102 |
| 76 76 77 78 78 79 79 79 | 80 80 81 81 81 82 82 88 83 72 97 96 99 100 101 101 101 103 163 |
| 52 53 77 77 78 78 78 79 79 80 80 80 | 81 82 82 82 85 83 83 83 74 88 99 100 100 101 101 102 103 103 |
| 52 53 53 53 54 55 56 56 56 80 81 92 93 94 95 96 97 92 | 81 82 82 82 82 82 83 84 84 76 |
| 52 58 53 54 55 55 55 56 56 77 78 78 79 79 80 81 81 81 81 91 92 93 84 93 96 96 97 98 | 57 58 59 59 59 60 60 60 60 81 82 82 83 83 84 84 85 85 78 99 100 100 100 101 102 103 104 105 |
| 62 63 54 55 55 56 56 67 78 79 80 80 81 81 82 82 82 82 82 96 97 98 99 99 | 88 58 59 59 59 60 90 60 61 61 80 83 83 84 84 85 85 85 85 86 86 80 90 101 101 102 103 104 104 105 106 |
| 46 48 50 52 54 56 58 60 62 | 64 66 68 70 72 74 76 78 80 |
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| | | | | | | | | | | | | | | | | | | -11 |
|-----------------|------------------|-------------------|-----------------|--------------------|------------------|--------------------|-----------------|-----------------------|------------------|-------------------|------------------|------------------|------------------|------------------|------------------|-------------------|--------------------|-----|
| 46 | 48 | 50 | 52 37 | 54 38 | 56 28 | 58 | 60 | | | | AS | HE | NH | UF | RST | "S | • | I |
| 44 63 | 44 68 | 45 68 | 45 64 | 46 64 | 47 64 | 47 | 48 88 | 10 | | Clo | th | Sti | uct | ure | T | able | es. | |
| 49 | 49 67 | 49 68 | 50 68 | 50 69 | 50 50 | 51 69 | 51,70 | 12 | | | | (0 | OFTRIO | efed) | | | inah i | |
| 51 70 | 51 | | 51 ₇ | | 52 72 | 72 | 53 78 | 14 | a C | r naa: Cloth i | ing to in any | comb | guer ioatio | not c | reaus ounts | orma per | inch in terials | : ∦ |
| 54 73 | 54 ₇₈ | 54 ₇₄ | 54 74 | 1 55 ₇₅ | 1155 75 | 56 ₇₆ | 56 76 | 16 | | | | _ | | | | | | |
| 56 76 | 56 76 | 44 57 77 | 44 57 77 | | 57 78 | 58 79 | 58 79 | 18 | | | Æ | 4 1 | n t | r | г | | | |
| 58,78 | 5979 | 46 59 79 | 59 80 | 59 80 | 60 _{B1} | 60 82 | 61 82 | 20 | | | Ţ | A | R | Ľ | E | 5, | | |
| 61 80 | 61 81 | 61 91 | 8.3 | 83 | 62 63 | 62 | 63 | 22 | C | | | | | | | | and | ı |
| 62 82 | 62 83 | 48 63 83 | 63 84 | 64 85 | 64 85 | 65 86 | 65 86 | 24 | | Cot | tton | or | Spu | n S | ilk | We | ft. | |
| 48 64 84 | 64 ₈₅ | 65 B5 | 65 85 | ⁶⁶ 66 | 5! 68 88 | 51 5 66 88 | 66 | 26 | | | | | | | | | | _ |
| 65 85 | 66 87 | 66 87 | 67 88 | 67 89 | 68 89 | 52 69 50 | 200 | 28/62 | 64 | 66 | 68 | , | - | | 76 | - 1 | 80 | _ |
| 67 87 | 68 | 5! 68 90 | 69 90 | 70 ₉₁ | 71 92 | 71 98 | 71 93 | 72 | 72 ₉₅ | 5 72 95 | | 72 96 | | | 7397 | G 16 | - 99 | 30 |
| 69 | 70 90 | 70 91 | 71 92 | 55 71 93 | 72 94 | 72 | 72 | 73 | 73 | 74 97 | 74 97 | 74 98 | 98 | 75 | 75 | 75 | 78 100 | 32 |
| 52 71 90 | 71 91 | 58 72 92 | 72 | 73 | 55 78 95 | 74 95 | 74 | 74 | 75 97 | 75 98 | 75 99 | 75 99 | 75 | 101 | 76 101 | 76 102 | | 34 |
| 73 | 73 93 | 54 73 94 | 54 74 96 | 55 74 96 | 95 75 96 | 75 | 76 | 76 | 76 | 77 | 77 | 8 0 77 100 | 77 | 78 101 | 78 | 78 | 79 103 | 36 |
| 54 74 93 | 75 lit | 75 | 75 | 76 | 78 | 77 | 77 | 98 57 77 100 | 77 | 78 101 | 78 | 78 | 78 | 79 104 | 79 6 | 0 6 79 105 | 80 106 | 38 |
| 76 94 | 76 96 | 77 | 56 77 98 | 57 78 98 | 78 | 78 | 79 | 79 101 | 79 | 80 | 80 | 81 | 81 104 | 81 | B1 105 | 81 106 | 107 | 40 |
| 77 | 78 97 | 56 79 98 | 79 | 79 100 | 58 79 160 | 79 | 80 | 80 103 | B0 104 | 81 105 | 81 105 | 82 | 82 108 | 82 | 83 | 83 108 | 109 | 42 |
| 58 78 97 | 79 98 | 79 | 80 100 | 80 100 | 81 10 | 81 102 | 61 103 | 82 104 | 82 105 | 82 105 | 83 | 83 106 | 83 108 | 84 108 | 84 | 84 109 | 110 | 44 |
| 36 79 98 | 80 100 | 80 190 | 81 101 | 82 102 | 82 101 | 82 :04 | 82 105 | 83 105 | 83 | 83 107 | 84 107 | 84 | 3 6 84 109 | 85 109 | 85 110 | 86 | 123 | 46 |
| 80 96 | 81 106 | 61 101 | 82 102 | 82 103 | 83 104 | 60 83 103 | 84 106 | 84 106 | 85 107 | 85 108 | 85 109 | 86 | 86 | 86 | 88 | 87 | 113 | 48 |
| 82 100 | 82 101 | 63 102 | 83 103 | 84 103 | 84 105 | 85 106 | 85 | 86 | 86 108 | 86 109 | 86 | 87 111 | 1111 | 87 | 88 | 88 | 88 | 50 |
| 82 101 | 83 102 | 93 102 | 60 B4 104 | 85 105 | 85 85 186 | 86 107 | 96 i 08 | 87 108 | 87 109 | 87 110 | 88, | 88,, | 89 | 89 | 89,14 | 89 | 90 | 52 |
| 84 102 | 84 103 | 85 103 | 61 85 105 | 86 106 | 86 107 | 62 87 108 | 87 109 | 88 110 | 88 | 88 112 | 89 112 | 89 | 90 | 90 114 | 90 | 91 | 91 | 54 |
| 84 108 | 85 104 | 85 105 | 86 106 | 87 107 | 63 58 108 | 63 89 109 | 89 110 | 64 89 111 | 89 112 | 89 113 | 80 114 | 90 | 91 115 | 91 116 | 92 117 | 92 | 93 | 56 |
| 85 104 | 86 101 | 86 106 | 86 86 107 | 62 87 108 | 63 88 109 | 68 89 110 | 90 111 | 91 112 | 91 113 | 91 114 | 92 114 | 92 115 | 92 | 92 115 | 93 | 93 | 94 | 58 |
| 87 105 | 87 100 | | 62 88 108 | 65 88 109 | 89 110 | 89 111 | 90 112 | | 91 114 | 92 114 | 93 116 | 93 | 93 | 117 | 94 119 | £5 119 | 95 120 | 60 |
| 88 106 | 89 (01 | 89 107 | 63 89 108 | 89 310 | 90 111 | 90 112 | 91 113 | 92 114 | 93 | 93 116 | 94 | 94 | 95 118 | 95 | 95 | 96 | 96 | 62 |
| 88 106 | 82 89 10 | 90 108 | 63 90 109 | 91 111 | 91 112 | 65 91 113 | 92 114 | 93 115 | 94 116 | 95 113 | 95 118 | 95 115 | 96 | 96 120 | 96 121 | 97 122 | 97 | 64 |
| 89 107 | 89 10 | 53 91 109 | 91 110 | 92 112 | 92 | 65 92 114 | 93 114 | 94 116 | 95 11: | 95 118 | 96 119 | 97 | 97 | 97 | 97 122 | 98 123 | 99 | 66 |
| 91 107 | 92 10 | 92 | 64 93 111 | 93 112 | 65 93 | 66 94 114 | 67 94 116 | 67 96 117 | 68 96 118 | 68 96 | 96 119 | 97 120 | 98 | 98 122 | 98 | 99 | 100 124 | 68 |
| 83 92 108 | 93 11 | | 93 111 | 94 113 | 66 94 114 | 56 95 115 | 96 116 | 68 97 118 | 97 118 | 97 120 | 98 120 | 95 121 | 99 122 | 99 123 | 99 | 100 124 | 101 125 | 70 |
| 63 92 106 | 93 | 64 94 0 111 | 65 95 11 | 95 114 | 96 115 | 67 96 116 | 68 97 117 | 98 115 | 69 98 119 | 98 120 | 70 99 121 | 99 122 | 100 | 100 | 100 124 | 101 125 | 101 128 | 72 |
| 98 | 84 94 11 | 65 95 112 | 65 96 118 | 97 114 | 97 1 316 | 98 116 | 98 117 | 99 119 | 69 99 120 | 70 99 121 | 100 122 | 100 128 | 100 123 | 101 | 72 101 125 | 101 | 102 136 | 74 |
| 710 | 95 | 65 96 1 112 | 86 97 | 66 88 | 67 98 111 | 68 99 117 | 68 99 117 | 1.0 | 100 (2) | 70 100 122 | 101 (23 | 101 124 | 101 125 | 101 125 | 102 | 102 126 | 102 137 | 76 |
| 96 | 65 96 | 97 2 11 | 66 98 | 87 99 110 | 68 99 6 11 | 69 100 7 118 | 69 100 | 101 121 | 70 101 122 | 70 101 123 | 71 102 128 | 72 162 (24 | 72 102 125 | 75 103 125 | 73 103 126 | 7.3 103 127 | 103 128 | 78 |
| 84 95 | 65 96 | 85 97 3 | 98 11 | 68 99 6 11 | 99 | 8 111 | 100 120 | 70 101 121 | 70 101 128 | 102 13 | 71 102 184 | 72 102 125 | 103 126 | 103 187 | 104 128 | 75 104 129 | 105 130 | 80 |
| 46 | 48 | 50 | 52 | 54 | 56 | 58 | 60 | 62 | 64 | 66 | 68 | 70 | 72 | 74 | 76 | 78 | 80 | |



| OF V | VA | RP. | | | | | | | | | | | - | | - | | | |
|----------------------------|-------------------|------------------|------------------|------------------|------------------|-----------------------|------------------------|-----------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|----------------|------------------------|----------|
| 46 | 48 | 50 | 52 | 54 | 56 | 58 | 60 | | | | | | | | | | | |
| 31 37 | 37. | 38 | 82 38 | 32 38 | 82 38 | 85 38_ | 33 | 10 | | ۰. | | | | | RS′ | | | |
| 33 40 | 40 | 84 84 | 84 41 | 84 41 | 84 41 | 35 41 | 38 41 | 12 | ŀ | Cl | oth | St | ruc | tur | e . | Fab l | les. | |
| 85 3 43 | 43 | 36 44 | 58 44 | 36 44 | 36 44 | 97 44 | 37 45 | 14 | | | | | | | | s per | | |
| 87 45 | 45 | 37 46 | 38 46 65 | 38 46 | 36 46 | 38 46 | 39 47 | 16 | a | Cloth | in any | y com | bioati | on of | COUAL | s or m | aterial | S. |
| 88 47 | 47 | 39 48 | 39 48 | 39 48 | 39 48 | 40 | 49 | 18 | | | | | | | _ | | | Ì |
| 50 88 | 50 | 50 ₇₀ | 51 70 | 51 70 | 52 71 | 53 ₇₂ | 54 78 | 20 | | | T | ΊA | Bl | LE | (| J. | | |
| 52 71 | 52 | 52 72 | 53 72 | 53 ₇₈ | 53 74 | 54 ₇₅ | 45 55 ₇₆ | 22 | | otto | | | | | | Zarp | an | ı |
| 42 54 78 | 54 | 54 74 | 55 74 | 55 ₇₅ | 55 ₇₅ | 44 55 76 | 45 56 | 24 | | | | | - | | /eft | • | | |
| 13 55 74 | 55 ₇₅ | 55 76 | 56 76 | 56 ₇₆ | 56 ₇₇ | 56 78 | 45 56 79 | 26 | | | | | | | | | | |
| 57 77 | 67 | 57 78 | 45 58 78 | 58 ₇₉ | 58 ₇₉ | 58 80 | 59 _{gn} | 28/ 62 | 64 | 66 | 68 | 70 | 72 | 74 | 7,6 | 78 | 80 | |
| 59 78 | \$9 ₇₉ | 58 ₇₀ | 59 80 | 46 60 81 | 60 81 | 60 82 | 60 87 | 48 60 83 | 46 61 89 | 46 61 84 | 49 61 84 | 61 64 | 49 61 85 | 49 61 85 | 62 88 | 62 62 | 62 87 | 30 |
| 59 80 | 60 ₀₁ | 60 81 | 60 82 | 48 60 82 | 61 83 | 62 83 | 48 62 84 | 62 65 | 63 ₈₅ | 63 86 | 30 63 84 | 63 ₈₇ | 63 87 | 63 | 64 88 | 51 64 88 | 64 88 | 32. |
| 61 ₈₁ | 61 82 | 61 82 | 61 | 62 83 | 62 84 | 63 86 | 63 85 | 63 | 50 64 86 | 64 ₈₇ | 64 87 | 51 64 88 | 64 ₈₉ | 65 86 | 65 90 | .65 90 | 65 ₉₀ | 34 |
| 62 63 45 | 63 53 | 63 ₈₄ | 63 85 | 64 85 | 64 ₈₆ | 50 64 87 | 65 ₈₇ | 50 65 88 | 51 65 88 | 3165 89 | 66 | 88 | 68 ₉₀ | 66 ₉₀ | 67 91 | 53 67 91 | 53 67 92 | 36 |
| 64 84 | 65 ₈₄ | 65 85 | 49 65 86 | 65 87 | 66 87 | 66 88 | 66 | 66 | 87 90 | 67 ₉₀ | 67 | 67 91 | 68 | 68 ₉₂ | **68 92 | 68 93 | 54 68 94 | 38 |
| 66 | 66 86 | 66 ₈₆ | 66 66 87 | 67 88 | 67 89 | 67 89 | 68 90 | 52 68 90 | 68 | 33 68 91 | 89 ₉₂ | 69 | 69,3 | 69 | 69 | 55 70 54 | ⁵⁵ 70 95 | 40 |
| | 67 84 | 67 67 | 67 88 | 68 | 32 68 90 | ⁵² 69 | 69 | 69 92 | 33 69 | 53 69 98 | 54 70 99 | 70 84 | 70 94 | 70 95 56 | 70 95 | 36 71 46 | 71 ₉₆ | 42 |
| 68 87 | 68 88 | 51 69 89 | *69 89 | 69 90 | | 53 70 | 70 70 92 | 53 70 93 | 34 70 | | 71 95 | 71 | 71 ₉₆ | 71 94 | 12 ₉₇ | 37 72 97 | 72 98 | 44 |
| 69 | 69 89 | 52 70 90 | 58 70 80 | 70 91 | 53 71 92 | 71.98 | 54 71 83 | 54 71 94 | 55 71 95 | 55 72 95 | 72 96 | 72 97 | 73 | 73 57 | 73 96 | 57 73 98 | 73 90 | 46 |
| 70 88 | 70 90 | 70 91 | 53 71 91 | 71 92 | 53 72 93 | ⁷² 94 | 54 72 95 | 55 72 95 | 33 73 96 | 73 97 | 73 98 | 56 73 98 | 74 99 | 74 99 | | 74 100 | 75 100 | 48 |
| 52 70 88 | 71 90 | 63 71 92 | 58 72 92 | 72 93 | | 73 95 | 73 96 | 74 97 | 56 74 98 | 36 74 98 | 74 99 | 57 75 99 | 75 100 | 75 100 | 78 101 | 76 | 76 102 | 50 |
| 71 96 | 71 91 | 53 72 92 | 73 ₉₃ | 73 M | 74, | 74 96 | 74 97 | 75 98 | 56 75 99 | 37 75 90 | 75 99 | 76 100 | 59 | 133 | 77 | 77 | 78 103 | 52 |
| 72 | 72 92 | 73 ₉₄ | 74 95 | 74 96 | 75 97 | 75 97 | 75 98 | łsg – | 37 76 99 | 78 190 | | 77 101 | 77 101 | 78 | 78 | 79 | 79 105 | 54 |
| 73 92 | 74 ₉₃ | 74 94 | 74 95 | 75 96 | 75 97 | 76 98 | 76 99 | 76 99 | 58 76 100 | 59 77 101 | 77 101 | 76 102 | 78 103 | 79 60 | 79 10- | 79 105 | 80 105 | 56 |
| 74 | 75 94 | 55 75 95 | 56 75 98 | 56 76 9; | 37 76 98 | 57 78 99 | 38 76 100 | 58 77 100 | | | 59 78 102 | | 79 104 | 80 10- | 80 | 80 61 | 91 107 | 58 |
| 74 93 | 75 ₉₄ | 55 75 95 | 56 75 96 | 56 76 97 | 76 96 58 | 56 76 100 | 58 77 101 | 78 101 | 78 101 | 79 108 | en . | 80 104 | 80 104 | 80 10: | 80 62 | 81 62 62 | 82 69 | 60 |
| 93 74 94 | 75 95 75 | 56 75 96 | | 57 76 98 | 58 76 99 | 58 77 100 59 | | 79 102 | 79 106 | 80 104 | 41 | 81 108 | | 81 10 | 62 61 62 | 82 108 | 83 109 | 62 |
| 75 90 | | 76 97 | 78 98 | i ii | INA | | 78 102 | 80 103 | 60 60 | 81 61 61 | 81 | 81 (06 | 81 ₁₀ | 82 10 | 82 82 10 | | 83 | 64 |
| 55 76 95 | 76 97 | 57 96 | 78 94 | 78 100 | 79 101 | 80 102 59 | 80 103 60 82 | 81 104 | 81 104 | 81 10: | 82 106 | 82 101 | | 83 10 | | 84 | 84 | 66 |
| 55 77 56 58 78 | 77 98 | 57 78 90 | | 80 100 | 59 81 101 | | 46 | 82 104 | | 7 | | | 68 84)0 | 84 10 | 164 | 85 | 85 311 | 68 |
| 134 | 76 98 | 57 57 | 79 100 | 50 | 81 102 | 81 60 | - | 82 105 | 83 101 | 83 | 40 | 85 101 | 85 104 | | 86 | 86 1 111 | 86 112 | 70 |
| 78 97 56 | 78 99 | 79 100 | 158 | 81 101 59 | 82 103 | 82 104 | 83 | 83 | 84 10 | - | 82 | 86 | 86 114 | 84 | 87 85 65 | 87 1 115 | 87 113 | 72 |
| 78 97 | 79 99 | 79 100 | 80 101 58 | 81 102 58 | 82 104 | 82 104 | 83 101 | 83 | 84 10' | | 85 109 | 96 316 | 87 | 87 11 65 | 88 1 85 | 88 | 88 114 66 | 74 |
| 78 98 | 79 99 | 164 | 58 81 101 | 160 | 83 104 | 83 165 | | 84 107 | | | 88 110 | 87 116 | 88 11 | 68 11 | 86 66 | 69 3 114 | 89 115 | 76 |
| 79 98 | 80 160 | 81 101 | 82 104 | 83 104 | 83 100 | 84 100 | 84 | 88 | 68 | Bu . | 164 | W- | 88 11 | 88 11 | 89 11 86 | 89 8 114 | 90 115 | <u> </u> |
| 80 | 361 | 191 | 83 | 84 | 84 | 85 | 86 | 88 | 87,0 | 87 | | 88 | 89 | 89 | 90 | 5 11 | 91 | 80 |
| 46 | 48 | 50 | 52 | 54 | 56 | 58 | 60 | 62 | 64 | 66 | 68 | 70 | 72 | 74 | 76 | 78 | 80 | ويسا |

| | | | | | | T | A | В | I. | E | ; | E | | | | | | | |
|------|------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|----------------------|------------------------------|--------------------------|-----------------------|----------------------|----------------------|----------------------|--------------|----------------------|----------|----------------------|
| _ | | | | For | Cc | | | | | | | | n ' | Wef | t. | | _ | | |
| ľ | | 10 | 12 | • | 1/ | -1 | - | | | 2/ | 28 | 30 | 32 | 34 | 36 | 38 | 40 | \dashv | 1 |
| } | | 10 | 12 | | 16 | 18 | 20 | 22 | 24 | 26 | 83 | 85 | 85 | 8.5 | 187 | 18.9 | 19 | | 11.5 |
| | 1 | 18.5 27 | 18.7 28 | 29 t | 29.6 | | 30 8 | 31 | 19 9 31 2 20.4 | 208 | 817 | 20 2 32 | 32 1 | 20 4 32 3 | 32 5 | | 20 6 23 1 | 1 | 14.7 20 |
| | 12 | 22.4 32.1 | 22 2 32.6 | 22 33 | 22 3 34 | 22 6 35 | 22 9 25 8 | 23.1 35 6 | 23 2 35 9 | 23 4 | 23.5 36 6 | 23 7 | 23 8 37 2 | 24 | 37 6 | | 25 6 38.2 | 15 | 15.8 |
| | 2 | 20.3 24.3 35.2 | 20 9 24 7 36.2 | 21.5 25.1 37.3 | 25 5 38 1 | 25 9 | 26 2 30 5 | 265 | 26 6 | 26 8 | 27 | 27 3 | 27 5 42 3 | 42 0 | 28 7 42 9 | 29.8 43.1 | 30 9 43 s | 2 | 16.4 23.7 |
| - | 21 | 21.4 25.9 | 22.1 26.5 38.4 | 22.9 27.1 39.7 | 27 6 1 | 28 41 5 | 28.3 42.2 | 28 6 42 9 | 24 9 28 8 43 6 | 25 t 29 1 44 | 5 6 29 3 44 5 | 29 6 | 29 8 | 30 45.8 | 26.7 30 6 46 | 312 | 31 8 46 f | 212 | 14.1 17 24.4 |
| ţ | 3 | 22 6 27 6 | 23 4 28 3 | 24.8 | 29.6 | 30.1 | 30.4 | 26 3 30 7 45 7 | 26.7 | 31 4 | 7 4 | 27 6 32 | 28 32 2 48 6 | 25.3 32.4 49 | 28 5 32.5 49.4 | 32 6 | 26 9 32 8 50 1 | 3 | 17.6 17.3 25.3 |
| ŀ | 3¦ | | 30.2 | 42.1 25.4 30.8 | | | 44 9 27 1 32 2 | | | 28.4 33.4 49.4 | | | 29 5 34 1 51 1 | | 20 | 30 3 34 7 | 30 5 34 9 52 8 | 31 | 17.8 26 |
| ł | 4 | 30 9 | 32.2 | 32.5 | 33 | 33 6 | 28 4 34 49.3 | 29 34 6 | 29 4 34 9 | | | 307 | 36.1 53.7 | 313 | 38 6 | 36 8 | 32 t 37 t 55 t | 4 | 15.7 18.4 26.6 |
| Ė | 41 | 49.8 35.4 32 | 24.3 32.7 | 33 5 | 34 | 34 6 | 35.2 | 35.9 | 36.2 | 36.6 | 37 | 31 8 37 4 55 I | 37 6 | 37 9 | | 33 38 3 | 33 3 38 8 57 8 | 41 | 18.5 18.5 |
| Ž | 5 | 26.1 33.2 | 45.7 27 33.6 | 34 9 | 35 2 | 50 9 2 35.5 | 30.1 36.4 52.7 | 31 37 4 | 37.9 | 38 2 | 38 7 | 39 | 39 2 | 33 6 | 39 9 39 7 | 34.2 | 34 5 40 1 59 8 | 5 | 18.5 |
| Ŀ | 5 <u>1</u> | 45.8 96.7 94 | 27.8 35 | 38.9 36 | 36 6 | 37 37 | 31 4 38 3 | 32.1 39 | 32 6 39.3 | 53 39 6 | 40 | 23 9 40 3 | 40 5 | 41 | 35 41 2 | 85.3 41.4 | 35.5 41.7 | 51 | 16.1 18.5 |
| 0 8 | 6 | 48.6 37.3 35 | 48.2 28.4 36 | 50.1 | 51 8 30 1 38 | 52 2 31 5 38 9 | 32 4 39 7 | 40.5 | 38 6 40 7 | 33 9 41 | 41 5 | 35 42 | 35 4 42 2 | 35 8 42 5 | 36 t 42 8 | 36 4 43 | 35 8 43.3 | 6 | 16 4 |
| ž | | 47.4 28 35.4 | 49 3 | 51.3 | 53 9 | 54.5 | 56.2 | 58 | 58 4 84.7 | 58 8 | 59 7 | 36 2 | 9) 3 | 9.0 | 37 4 | | 63 8 38 2 45 2 | 61 | 16.6 19 |
| COUN | 61 | 48.7 28.8 | 20 5 | 31 1 | 32 2 | 33.6 | 57 6 34 2 | 59 4 35 1 | 35 7 | 60 B | 61 9 36 B | 62 8 37 4 | 63 5 | 38 4 | 38 8 | 65 6 | 66 2 39 6 47 2 | 7 | 16.7 19 1 |
| | 7 | 35 8 50 | 30.2 | 31.4 | \$6 32.5 | 33 7 | 59 4 34 5 | | | 44.5 62.9 36.5 | 45 63 7 | 65 | 65.8 | 46 4 66 6 | 39 2 | 39.7 | 40 | 71 | 17 |
| П | 71 | 37 50 1 | 38.5 52.4 | | 55.3 | 42,3 | 43 | 43.9 6) 2 | 44.4 62.5 | 36.5 44.9 68.5 36.9 | 45 4 64 5 37 5 | 45 9 65 5 38. i | 46 4 46 3 | 46 7 67 2 | 47 1 68 | 40 | 40 4 | 71 | 19.2 29 |
| | 8 | 38 3 50. | 39.5 | 40 8 55.2 | 41 8 57 | 42 8 58 9 | 43 5 60 8 35 3 | 44.3 | 44 8 | 45 3 | 45 8 65 | 46 4 | 46 7 66 8 | 47 1 | 47 7 68 4 | 48 2 69 2 | 48.8 | 8 | 19 2 |
| | 81 | 29.6 39 51.1 | 40.3 | 41.6 | 42 6 88 | 43.6 | 44.6 | 45 6 | 46 63 8 | 37.5 46 3 65 | 46 8 | 47.4 | 47 7 | 48 1 68 8 | 48 6 | 49 | 496 | 8; | 19.3 |
| | 9. | 39.7 55 | 31 4 41 54. | 42 4 | 33.9 43.4 59.2 | 85 44.5 60.7 | 45 7 62.2 | 46.9 63.7 | 47 1 64 | 38 1 47 3 66 | 47 8 67 2 | 48 5 68.4 | 48 8 69 2 | 49.1 | 49 4 70 8 | 49 9 | 50 4 72 4 | 9 | 19.8 |
| | 91 | 80 3 40 4 52 | 32.7 41.7 | 38 2 43 1 57.5 | 44 2 | 35 6 45 4 | 36 1 46 3 63 | 37 2 47 3 | 138 | 38 7. 48 2 67 | 39 3 48 8 68.2 | 49 4 69 1 | 49 8 70 3 | 50 2 71 2 | 50 B | 51 72 6 | | 91 | 17.4 19.4 30. |
| | 10 | 30.7 | 32.8 42.4 | 33.6 43.8 | 144 4 | 463 | 47 | 97 a | 38 48 9 66 1 | 200.3 | 40 | 40 7 50 3 70 6 | 50 8 71 5 | 41 8 51 3 72.5 | 42 2 51 7 73 | 42 7 52 1 | 43 8 52 5 74 9 | 10 | 17.5 19.6 30 |
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| 14.1 18 24.5 | 19 26 3 | 10 8 97.6 | 20 1 | 20.5 29 6 | 20 9 | 21.2 | 21.4 | 18 6 21 8 32 2 | 22.2 32.7 | 19.2 22.4 33.1 | 19 5 22 6 33 5 | 19 6 22 8 34 | 22.9 34.2 | 22 3 34 6 | 19 8 23.1 14.8 | 23.2 25.1 | 20 4 23 3 35 4 | 11 |
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| 19.8 27.6 | 17 2 21 7 29 8 | 22.8 | 23.9 32.8 | 24 4 33 6 | 25 35 | 20.7 25.4 36 | 21 2 25 8 36 8 | 21.6 26.2 36.4 | 26 5 38.1 | 22.3 26.7 39.2 | 22 7 27 39 4 | 27.2 39.9 | 23 4 27 5 40 4 | 23 6 27 7 40.8 | 23 8 28 41 2 | 24 28 1 41 6 | | 21 |
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| 21.8 32.2 | 24 3 | 26 2 | 28 | 29 5 | 31 | 32.1 | 33#2 | 33 6 | 34.1 | 34 6 | 35.1 | 35 8 | 36 1 | 36 5 | 37 | 37 5 | 31 38 51 3 | 5 |
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| 23 3 55.4 | 26 1 39.3 | 28.2 | 30.4 | 32 2 | 34 | 35 4 | 36 8 | 38 53 8 | 31.9 39.2 55.3 | 40.3 56 1 | 41.5 51.7 | 42 4 58 8 | 43.3 59.8 | 44 2 60 2 | 617 | 45 9 62,0 | 63 5 | 10 |
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